



Standard Radiometers and Targets for Microwave Remote Sensing

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IGARSS, Anchorage, 9/21/04



INTRODUCTION



- NIST microwave radiometry effort
 - Noise & antenna metrology have been conducted separately for over 30 years
 - Recently began doing remote-sensing radiometry, combining the two
- NIST Optical Tech. Div. has such a program for UV, Visible, & IR
- Developing analogous capabilities at microwave & mm-wave frequencies, providing a link between microwave remote-sensing measurements & NIST measurements & standards



- Calibration
 - linear radiometers \Rightarrow need (≥) two standards for calibration
 - need independent cal of targets, comparison to other radiometers, traceability
- Develop (& transfer) a standard for microwave brightness temperature
- Still in early stages, but some progress made

THEORETICAL FRAMEWORK



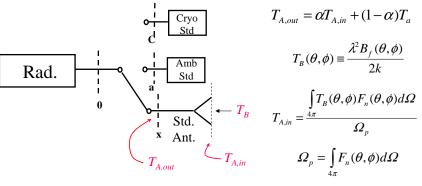
- Standard radiometer
- Brightness temperature
- Chamber
- Expected uncertainty



Standard Radiometer



• Radiometer measures $T_{A,out}$; want to determine T_B (assume far field conditions)



$$T_{A,out} = \alpha T_{A,in} + (1 - \alpha) T_a$$

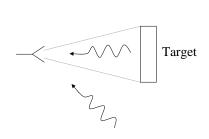
$$T_B(\theta,\phi) \equiv \frac{\lambda^2 B_f(\theta,\phi)}{2k}$$

$$T_{A,in} = \frac{\int_{A}^{B} T_{B}(\theta, \phi) F_{n}(\theta, \phi) d\Omega}{\Omega_{p}}$$

$$Q_{in} = \int_{A}^{B} F_{in}(\theta, \phi) d\Omega$$



• Break up $T_{A,in}$:



$$\overline{T_T} = \frac{\int\limits_{\text{target}} T_B(\theta,\phi) F_n(\theta,\phi) d\Omega}{\int\limits_{\text{target}} F_n(\theta,\phi) d\Omega}$$

$$\overline{T_{BG}} = \frac{\int\limits_{\text{other}} T_B(\theta,\phi) F_n(\theta,\phi) d\Omega}{\int\limits_{\text{other}} F_n(\theta,\phi) d\Omega} \ .$$

$$\eta_{AT} \equiv \frac{\int F_n(\theta,\phi) d\Omega}{\Omega_p}$$

$$T_{A,in} = \eta_{AT} \overline{T_T} + (1 - \eta_{AT}) \overline{T_{BG}}$$



• So,

$$T_{\scriptscriptstyle A,out} = \alpha \eta_{\scriptscriptstyle AT} \overline{T}_{\scriptscriptstyle T} + \alpha (1 - \eta_{\scriptscriptstyle AT}) \overline{T}_{\scriptscriptstyle BG} + (1 - \alpha) T_{\scriptscriptstyle a}$$

- Control the background, $\overline{T}_{BG} = T_a$
- Then

$$\overline{T_T} = T_a + \frac{1}{\alpha \eta_{AT}} \left(T_{A,out} - T_a \right)$$

• So we need $\alpha \approx 1/L$ and η_{AT}

$$\eta_{\rm AT} \equiv \frac{\displaystyle \int\limits_{\rm target} F_n(\theta,\phi) d\Omega}{\Omega_p}$$

• Will need a chamber to control background Temperature-monitoring Antibient Noise Radiometer Waveguide Radiometer Waveguide Standard Temperature Anticirculator Temperature Tem



Uncertainties



• Approximate achievable uncertainties:

$$u^{2}(\overline{T}_{T}) = \left(1 - \frac{1}{\alpha \eta_{AT}}\right)^{2} u^{2}(T_{a}) + \left(\frac{1}{\alpha \eta_{AT}}\right)^{2} u^{2}(T_{A,out}) + (\overline{T}_{T} - T_{a})^{2} \left(\frac{u^{2}(\eta_{AT})}{\eta_{AT}^{2}} + \frac{u^{2}(\alpha)}{\alpha^{2}}\right)$$

$$u(T_{a}) \approx 0.2 \text{ K}$$

$$u(T_{A,out}) \approx 0.3 - 0.5 \text{ K (for } T_{A,out} = 200 \text{ to } 300 \text{ K,}$$

18 - 26.5 GHz

$$u(\eta_{AT}) \approx 0.003$$

 $u(\alpha) \approx 0.005$

• So should be able to get

$$u(\overline{T}_T) \approx 0.3 \text{ K to } 0.7 \text{ K}$$

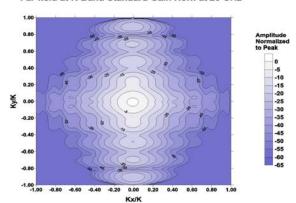
for $T_{A,out} = 200 \text{ to } 300 \text{ K}, 18 - 26.5 \text{ GHz}$

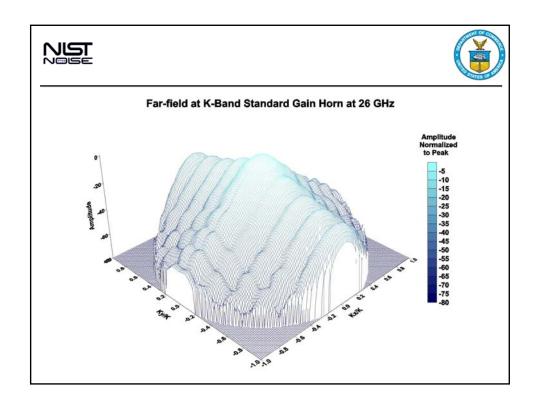
MEASUREMENTS (PRELIMINARY)



• Measured antenna pattern for a standardgain horn (SGH) on the near-field range

Far-field at K-Band Standard Gain Horn at 26 GHz



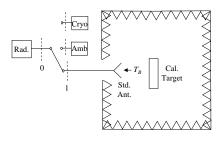




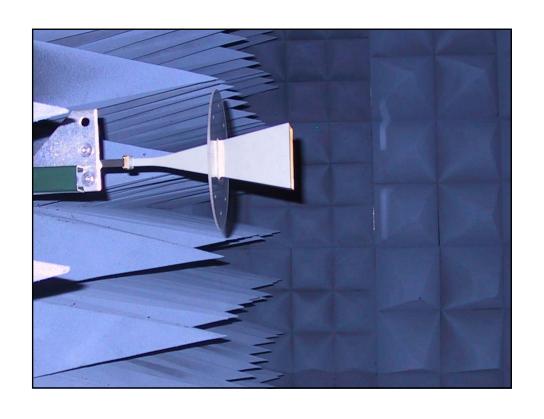
- Integrate pattern to get η_{AT} ; value depends on frequency & distance. At 26 GHz, $\eta_{AT} = 0.980$ at 50 cm, $\eta_{AT} = 0.301$ at 5 m
- Compute α from conductivity. $\alpha = 0.9954 \pm 0.0023$ at 26 GHz
- Connected SGH to the DUT plane of the WR-42 (18 26.5 GHz) waveguide radiometer



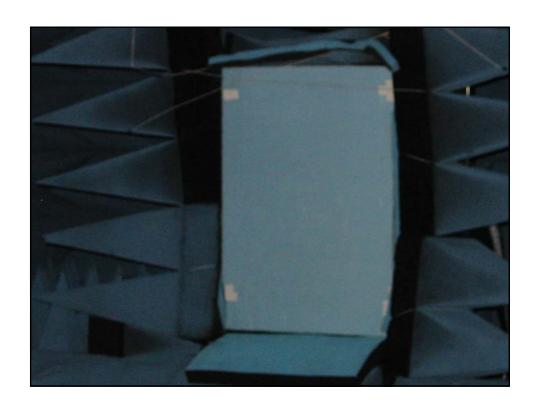
- Borrowed hot calibration targets from NOAA GSR (Al Gasiewski & Marian Klein, NOAA ETL) and NASA Goddard (Paul Racette)
- Measured it in the NIST anechoic chamber at 18, 22, & 26 GHz for several distances

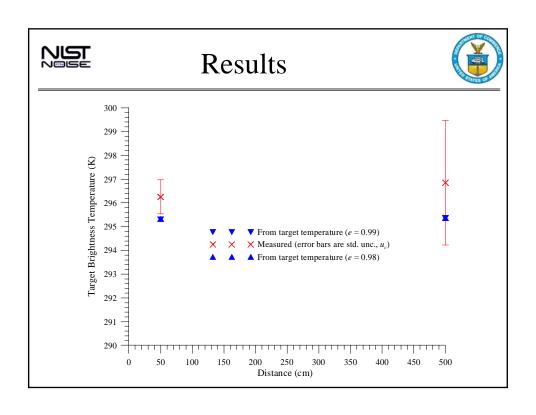


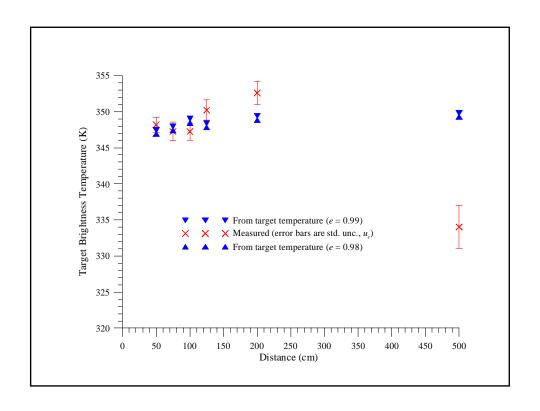






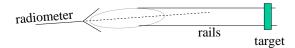




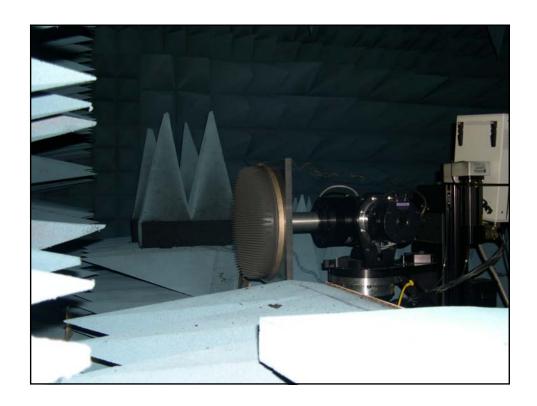




• 5 m results discrepancy probably just due to (mis)alignment



• Uncertainty large due to large $u(\eta_{AT}) = 0.0153$. Would be $u(\eta_{AT}) \approx 0.003$ if we knew target location better



Issues



- Type A uncertainties (target drift)
- Target location & angles
- Alignment of radiometer & target
- Near/Far field
- Emissivity: $T_T = eT_{target} + (1 e)T_{refl}$, e = ?



SUMMARY



- Developing a microwave (18 65 GHz) brightness-temperature standard based on existing noise standards and radiometers, plus antenna characterization
- Have developed framework and performed preliminary measurements
- Expect uncertainties of about 0.5 0.7 K for $T_B = 200$ to 300 K, f = 18 26 GHz (Larger uncerts for higher/lower temperatures and/or higher frequencies)



- Next:
 - Further preliminary measurements (different target)
 - Design & build special-purpose chamber
 - Measurements in special-purpose chamber
 - Measurements of a target in the IR using TXR radiometer
 - Develop standard target